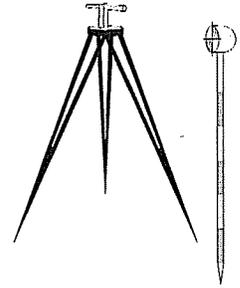




SPARACO & YOUNGBLOOD, PLLC
CIVIL ENGINEERING * LAND SURVEYING * SITE PLANNING
P.O. Box #818; 18 N. Main Street Harriman, N.Y. 10926
(845) 782-8543 Fax (845) 782-5901
sparaco.steve@selsny.com
wdyls1@gmail.com



August 21, 2024

Bernard Weintraub
92 Clinton Avenue
South Nyack, NY 10960

Re: 92 Clinton Avenue, South Nyack, NY 10960 – Drainage Report (YB-2725)
Section 66.54, Block 1, Lot #34.1

Dear Mr. Weintraub:

We have prepared a hydrologic analysis of the 0.44-acre 92 Clinton Avenue plot plan project located in the Town of Orangetown, NY.

It is proposed to construct a new 180-foot long, 10-foot wide driveway with turn around area to a proposed two-car garage which will serve a proposed 2-story frame single family residence at the site.

We have determined that drainage on this site generally drains towards from the South and West to one general collection point to the North and East of the site to an existing 42-inch RCP located along the properties Northerly boundary (Study Point #1).

For existing conditions, although this site had previously been developed in the past, we have evaluated this site as if it had been undisturbed for the purposes of this drainage report and to be conservative.

We have reviewed the Rockland County Soil Survey conditions for this area and have determined this site contains Wethersfield Soils (Hydrologic Group Type "C") in the proposed area of work.

We have determined that it is necessary to convey all roof drainage on site and the runoff collected in the proposed driveway on site to a new proposed detention system consisting of 90 LF of 60-inch diameter HDPE with an outlet structure and then discharge via 15-inch diameter pipe to the proposed 42-inch RCP located to the North of the site. The outlet structure will utilize a 2.25-inch orifice and 12-inch diameter overflow riser to route flows draining offsite to less than the existing conditions discharges.

Our analysis includes storms ranging from the 1-year to the 100-year design. Design frequencies were based upon Extreme Precipitation tables for the Northeast (reference: www.precip.eas.cornell.edu.com) for this site location.

Refer to the Summary Table below for a comparison of Existing and Developed Conditions Discharges from the site.

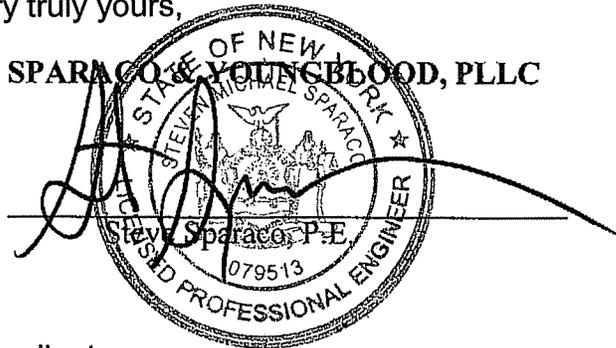
Summary Table # 1 – 92 Clinton Avenue Discharges just offsite to the North and East (Pt. #1) for Existing and Developed Conditions:

Conditions	Storm Frequency (in years)					
	1	2	5	10	25	100
Pre-Dev.t Discharges (cfs)	0.17	0.32	0.55	0.79	1.19	2.12
Post-Dev. Discharges (cfs)	0.17	0.27	0.44	0.59	0.84	2.02
Net Change:	-0.00	- 0.05	- 0.11	- 0.20	- 0.35	- 0.10

Attached are drainage area maps, drainage calculations and backup Hec-1 output data in support of our analysis.

Very truly yours,

SPARACO & YOUNGBLOOD, PLLC



cc.: client

TABLE OF CONTENTS:

- Drainage Narrative dated 8-21-18
- Table of Contents ^insert^

Appendix:

- 1.) *Methodology*
- 2.) *Figure A: Existing Conditions Drainage Area Map at 1"=30' scale*
- 3.) *Figure B: Developed Conditions Drainage Area Map at 1"=30' scale*
- 4.) *Figure C: Developed Conditions Plan View at 1"=20' scale*
- 5.) *Figure D: Outlet Structure Detail for the Detention System*
- 6.) *Rockland County Soils Information*
- 7.) *Curve Number Calculations*
- 8.) *Volume Calculations*

Hec-1 Analyses:

- 1.) *Cornell University 24-hour Precipitation Reference*
- 2.) *Existing Conditions Hec-1 Model*
- 3.) *Developed Conditions Hec-1 Model*

ENGINEERING METHODOLOGY:

Area Hydrology:

We have prepared a hydrologic analysis of the 0.44-acre 92 Clinton Avenue plot plan project located in the Town of Orangetown, NY.

Methodology:

We have determined that drainage on this site generally drains towards from the South and West to one general collection point to the North and East of the site to an existing 42-inch RCP located along the properties Northerly boundary (Study Point #1).

All drainage area delineations and any changes from existing to proposed conditions are indicated graphically on Drainage Area Maps provided in the Appendix.

A hydrologic analysis was performed utilizing procedures outlined in the Soil Conservation Service (SCS) publication Technical Report 55 (TR-55). SCS hydrographs were developed utilizing hydrographs consisting of a 24-hour rainfall event using an SCS Type-III rainfall distribution and unit hydrograph parameters, including drainage area, curve number (CN), time of concentration, and percent impervious.

Onsite time of concentration travel paths were insignificant and diminimus as they pertain to this project upon review of the area hydrology thru this site. A 10-minute minimum was used for existing conditions and a 5-minute minimum time of concentration was used for proposed conditions for all subareas on site.

Curve number calculations were based on hydrologic soil data obtained from available Rockland County Soils Maps. Refer to the Appendix for supporting soils data.

The Army Corps of Engineers hydrologic analysis computer program HEC-1 was utilized to generate runoff hydrographs for the 1, 2, 5, 10, 25 and 100-year frequency storms for pre and post-development conditions. This program was also utilized to perform hydrograph routings and additions to design the required mitigative facilities for developed conditions.

Stormwater Analysis and proposed mitigation:

It is proposed to construct a new 180-foot long, 10-foot wide driveway with turn around area to a proposed two-car garage which will serve a proposed 2-story frame single family residence at the site.

For existing conditions, although this site had previously been developed in the past, we have evaluated this site as if it had been undisturbed for the purposes of this drainage report and to be conservative.

We have reviewed the Rockland County Soil Survey conditions for this area and have determined this site contains Wethersfield Soils (Hydrologic Group Type "C") in the proposed area of work.

We have determined that it is necessary to convey all roof drainage on site and the runoff collected in the proposed driveway on site to a new proposed detention system consisting of 90 LF of 60-inch diameter HDPE with an outlet structure and then discharge via 15-inch diameter pipe to the proposed 42-inch RCP located to the North of the site. The outlet structure will utilize a 2.25-inch orifice and 12-inch diameter overflow riser to route flows draining offsite to less than the existing conditions discharges.

FRANKLIN STREET

150' WIDE ROW
150 MPH SPEED LIMIT

NO MARKING
NO PARKING
STOP SIGN
STOP SIGN
STOP SIGN

NO THRU TRAFFIC
30 MPH LIMIT
TRAFFIC SIGN
TRAFFIC SIGN

RAISED DOME DEFLECTION PADS

FLASHING TRAFFIC LIGHT

STRIAN WALK

15' ROW

FM LOCATION AS PER TOWN OF ORANGE DEPT. OF ENVIRONMENTAL MANAGEMENT AND ENGINEERING

N/V VILLAGE OF SOUTH NYACK L. 908, P. 357

TRAIL RULES SIGN FM ESPOSITO WALKING TRAIL

12" CRAB 12" APPLE

12' WIDE FENCE ROW

RET. WALL AS PART OF BUILDING

SITE-1
A=0.44 AC
I=0.00 AC

FENCE 0.02 AC

#90
2 1/2 STORY
FRAME DWL
TT-8822
TST-1907

EXISTING CONDITIONS
DRAINAGE AREA MAP
1=30'
8-21-24
FIGURE A

TEST MELL 41050100 667N E=8161

N/V CHURCHILL 66.62-1-1

BUILD COR 13.6' NE-COR

BUILDING

2 CAR GARAGE FRAME GARAGE

GARAGE

TEST MELL E-83.78

CHAIN LINK FENCE REMAINS

10' SYCAMORE

TEST MELL E-83.99

EASEMENT FM #910

9' WIDE ACCESS

0.3' N INV.-74.41

CHAIN LINK FENCE REMAINS

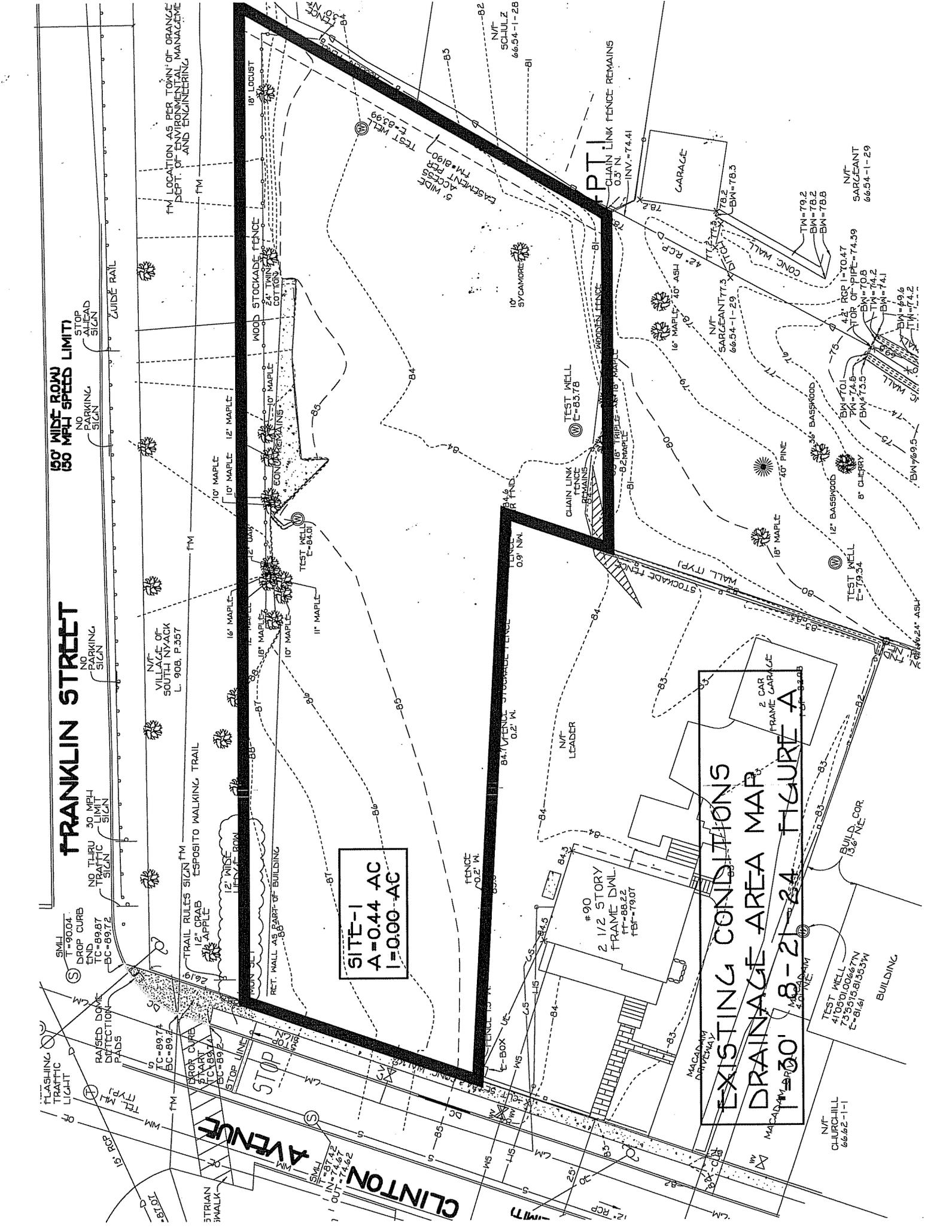
CONC. WALL

4.2' RCP

16' MAPLE 40' ASH

N/V SARGENT 66.54-1-29

4.2' RCP 1=70.47



FRANKLIN STREET

150' WIDE ROW
150 MPH SPEED LIMIT

NO PARKING
AHEAD
STOP SIGN

NO THRU TRAFFIC
LIMIT SIGN

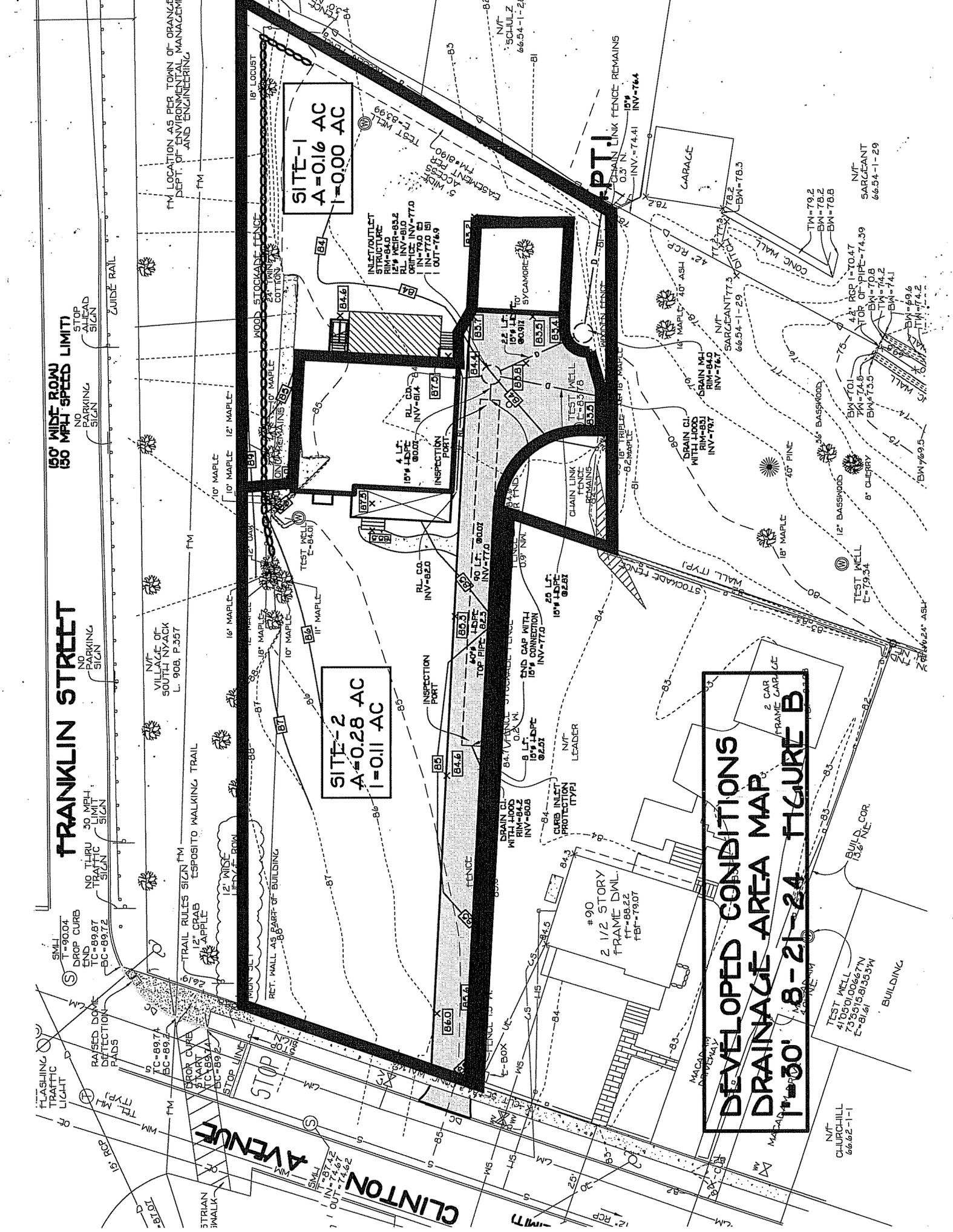
NO PARKING
SIGN

CLINTON AVENUE

DEVELOPED CONDITIONS DRAINAGE AREA MAP 1"=50' 8-21-24 FIGURE B

SITE-1
A=0.16 AC
I=0.00 AC

SITE-2
A=0.28 AC
I=0.11 AC



FM LOCATION AS PER TOWN OF ORANGE
DEPT. OF ENVIRONMENTAL PLANNING
AND ENGINEERING

18' LOCUST
24' TRINITY
COTTONWOOD

10' MAPLE
12' MAPLE
16' MAPLE
18' MAPLE

FM LOCATION AS PER TOWN OF ORANGE
DEPT. OF ENVIRONMENTAL PLANNING
AND ENGINEERING

18' LOCUST
24' TRINITY
COTTONWOOD

10' MAPLE
12' MAPLE
16' MAPLE
18' MAPLE

FM LOCATION AS PER TOWN OF ORANGE
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AND ENGINEERING

18' LOCUST
24' TRINITY
COTTONWOOD

10' MAPLE
12' MAPLE
16' MAPLE
18' MAPLE

FM LOCATION AS PER TOWN OF ORANGE
DEPT. OF ENVIRONMENTAL PLANNING
AND ENGINEERING

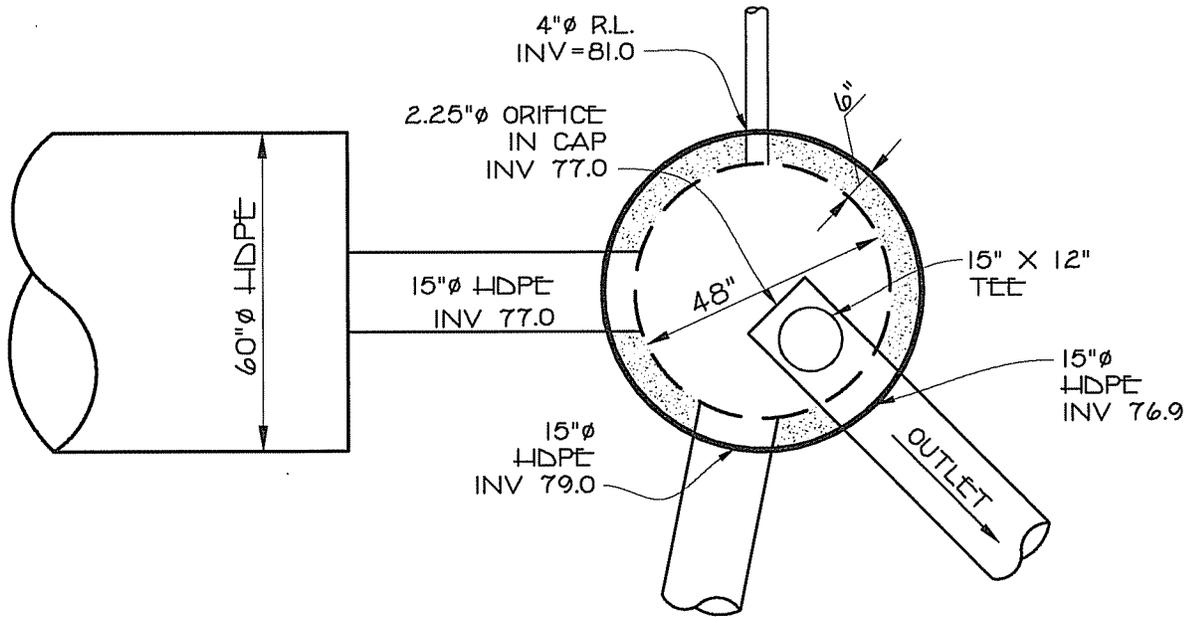
18' LOCUST
24' TRINITY
COTTONWOOD

10' MAPLE
12' MAPLE
16' MAPLE
18' MAPLE

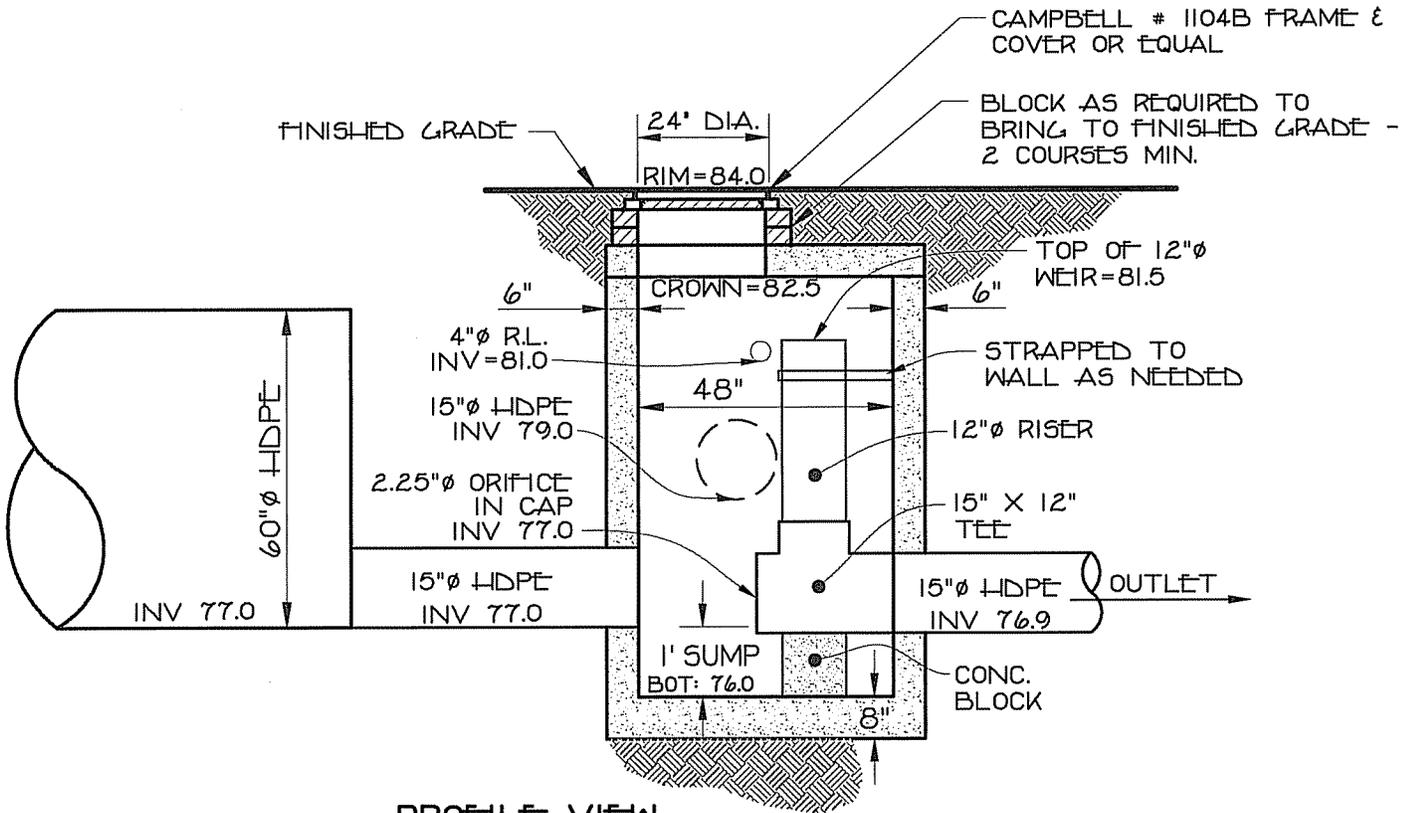
FM LOCATION AS PER TOWN OF ORANGE
DEPT. OF ENVIRONMENTAL PLANNING
AND ENGINEERING

18' LOCUST
24' TRINITY
COTTONWOOD

10' MAPLE
12' MAPLE
16' MAPLE
18' MAPLE



PLAN VIEW



PROFILE VIEW

INLET / OUTLET STRUCTURE

N.T.S

FIGURE D

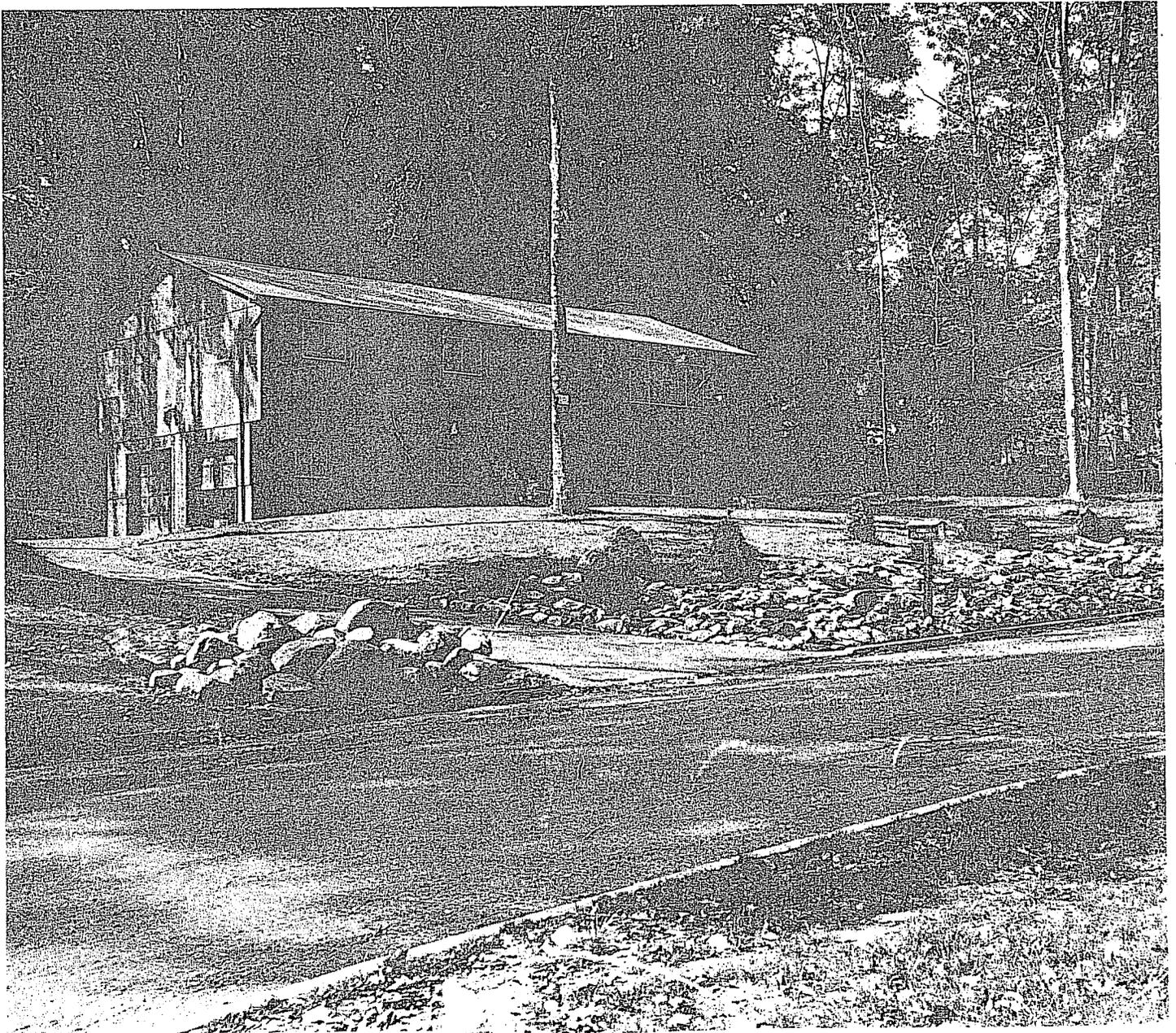
United States
Department of
Agriculture

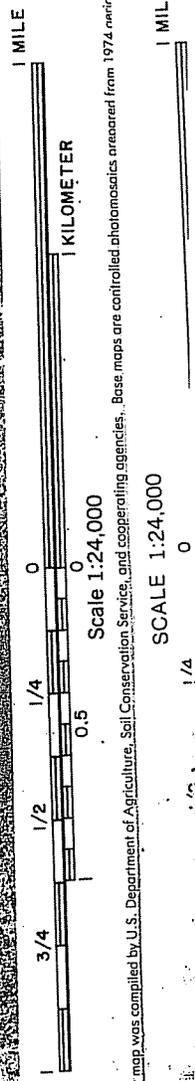
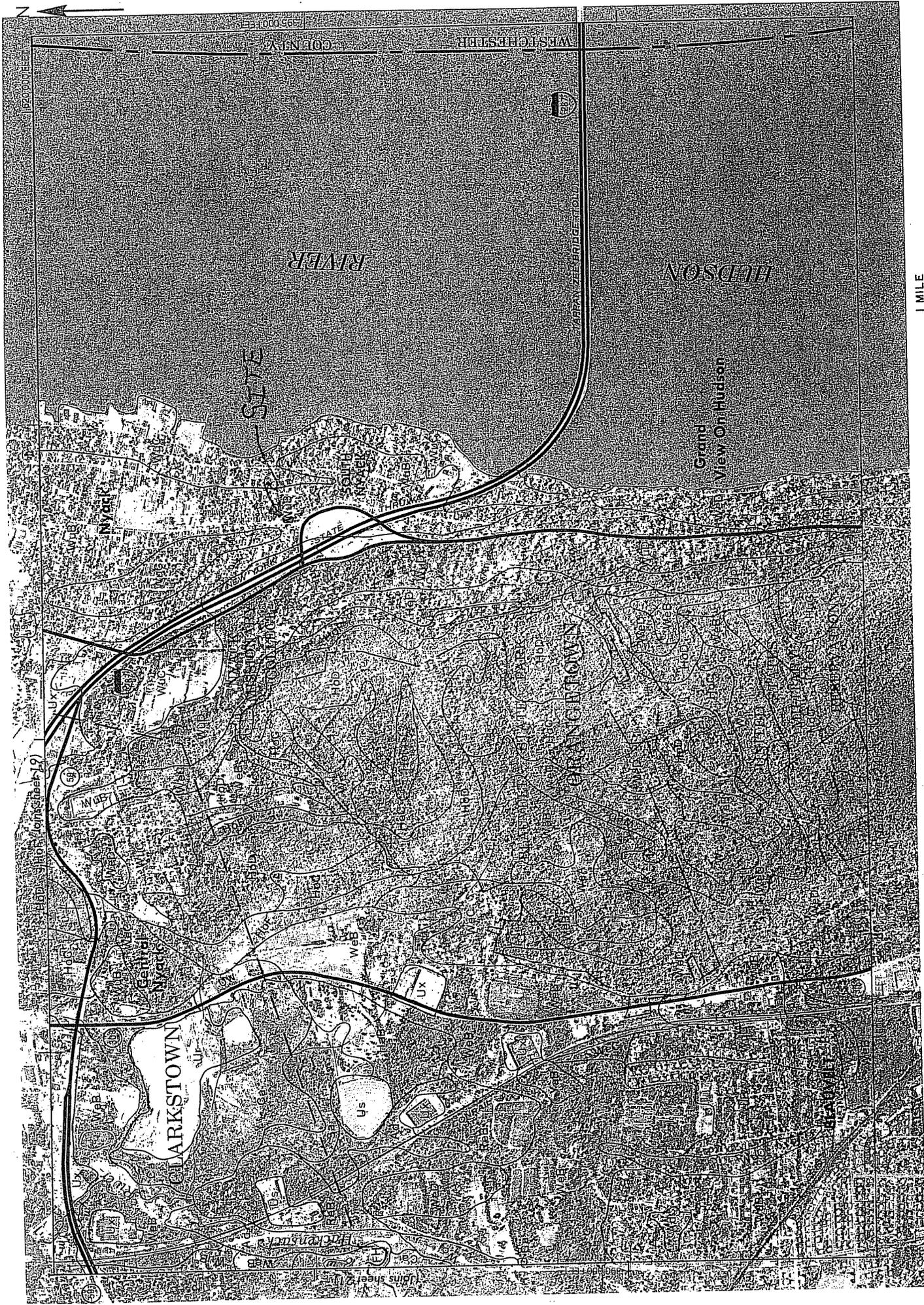
Soil
Conservation
Service

In cooperation with
Cornell University
Agricultural Experiment
Station

Soil Survey of Rockland County, New York

4B-2725
92 Clinton Ave.
South Nyack, NY
10960





This soil survey map was compiled by U.S. Department of Agriculture, Soil Conservation Service, and cooperating agencies. Base maps are controlled photomosaics arranged from 1974 period.

Scale 1:24,000
SCALE 1:24,000
1 MILE

TABLE 19.---SOIL AND WATER FEATURES---Continued

Soil name and map symbol	Hydro-logic group	Flooding			High water table			Bedrock		Risk of corrosion		
		Frequency	Duration	Months	Depth	Kind	Months	Depth	Hardness	Potential frost action	Uncoated steel	Concrete
Pl*, Pv*, Pits					<u>Ft</u>		<u>In</u>					
Ra, Rippowam	C	Frequent	Brief	Oct-May	0-1.5	Apparent	Sep-Jun	>60	---	High	High	High.
ReA, ReB, ReC, Red, Riverhead	B	None	---	---	>6.0	---	---	>60	---	Moderate	Low	High.
RuB*, RuC*, RuD*, Riverhead	B	None	---	---	>6.0	---	---	>60	---	Moderate	Low	High.
Urban land.												
Sa, Sloan	B/D	Occasional	Brief	Nov-Jun	0-1.0	Apparent	Nov-Jun	>60	---	High	High	Low.
Ur*, Us, Uw, Uorthents												
Ux*, Urban land												
Wa, Wallington	C	None	---	---	0.5-1.5	Perched	Jan-Apr	>60	---	High	High	Moderate.
Wc, Watchaug	B	None	---	---	1.5-2.5	Apparent	Nov-Apr	>60	---	High	Low	High.
WeA, WeB, WeC, WeD, Wethersfield	C	None	---	---	1.5-2.5	Perched	Feb-Apr	>60	---	Moderate	Low	Moderate.
WuB*, WuC*, WuD*, Wethersfield	C	None	---	---	1.5-2.5	Perched	Feb-Apr	>60	---	Moderate	Low	Moderate.
Urban land.												
YaB, YaC, YaD, Yalesville	C	None	---	---	>6.0	---	---	20-40	Hard	Low	Low	Moderate.
YuB*, YuC*, YuD*, Yalesville	C	None	---	---	>6.0	---	---	20-40	Hard	Low	Low	Moderate.
Urban land.												

* See description of the map unit for composition and behavior characteristics of the map unit.

SPARACO & YOUNGBLOOD, PLLC
 18 NORTH MAIN STREET
 HARRIMAN, NY 10926
 845-782-8543

Worksheet 2: Runoff Curve Number and Runoff

Project: 92 Clinton YB#2725

By: SMS

Date: 7-Aug-24

Location: 92 Clinton St., South Nyack

Checked:

Date:

Shade one: Existing Developed

CN for Sub-basin: Site-1

1. Runoff Curve Number (CN)

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area ■ acres □ mi ² □ %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0.44	30.8
C	Lawn / Open Space - Good Condition	74			0	0
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.00	0
Totals =					0.44	30.8

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{30.8}{0.44} = 70$

Use CN = 70

2. Runoff

Frequency..... yr.
 Rainfall, P (24 - hour) in.
 Runoff, Q in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm # 1	Storm # 2	Storm # 3

SPARACO & YOUNGBLOOD, PLLC
 18 NORTH MAIN STREET
 HARRIMAN, NY 10926
 845-782-8543

Worksheet 2: Runoff Curve Number and Runoff

Project: 92 Clinton YB#2725

By: SMS

Date: 7-Aug-17

Location: 92 Clinton St., South Nyack

Checked:

Date:

Shade one: Existing Developed

CN for Sub-basin: Site-1

1. Runoff Curve Number (CN)

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area ■ acres □ mi ² □ %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.16	11.84
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.00	0
Totals =					0.16	11.84

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{11.84}{0.16} = 74$

Use CN = 74

2. Runoff

Frequency..... yr.
 Rainfall, P (24 - hour) in.
 Runoff, Q in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm # 1	Storm # 2	Storm # 3

SPARACO & YOUNGBLOOD, PLLC

18 NORTH MAIN STREET
HARRIMAN, NY 10926
845-782-8543

Worksheet 2: Runoff Curve Number and Runoff

Project: 92 Clinton YB#2725

By: SMS

Date: 7-Aug-24

Location: 92 Clinton St., South Nyack

Checked:

Date:

Shade one: Existing Developed

CN for Sub-basin: Site-2

1. Runoff Curve Number (CN)

Soil name and hydrologic group (appendix A)	Cover Description (cover type, treatment, and hydrologic condition; percent impervious; unconnected / connected impervious area ratio)	CN			Area ■ acres □ mi ² □ %	Product of CN X AREA
		Table 2-2	Figure 2.3	Figure 2.4		
B	Woods - Good Condition	55			0	0
B	Lawn / Open Space - Good Condition	61			0	0
C	Woods - Good Condition	70			0	0
C	Lawn / Open Space - Good Condition	74			0.17	12.58
D	Woods - Good Condition	77			0	0
D	Lawn / Open Space - Good Condition	80			0	0
	Impervious Surfaces	98			0.11	10.78
Totals =					0.28	23.36

CN (weighted) = $\frac{\text{total product}}{\text{total area}} = \frac{23.36}{0.28} = 83.42857143$

Use CN = **83**

2. Runoff

Frequency..... yr.
Rainfall, P (24 - hour) in.
Runoff, Q in.

(Use P and CN with table 2-1, fig. 2-1, or eqs. 2-3 and 2-4.)

Storm # 1	Storm # 2	Storm # 3

SPARACO & YOUNGBLOOD, PLLC
 18 North Main Street, PO Box #818
 Harriman, NY 10926
 845-782-8543

Pipe Storage versus Elevation

Input:

Description Proposed *Pipe Area Equation when not full:*
 Detention structure for 92 Clinton YB# 2725 $\phi = \text{ARCCOS}((r-d)/r)$
 HEC-1: Route Where:

Basic Pipe Information (larger)

- 1. Pipe Size 60.00 Inches
- 2. Pipe Length 90.00 feet

Basic Pipe Information (smaller)

- 1. Pipe Size 77.00 Inches
- 2. Pipe Length 77.00 feet

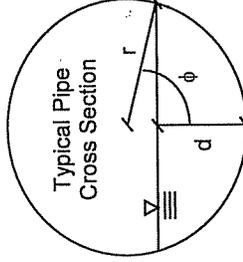
Storage Information

- 3. Invert of pipe 77.00 feet

$A = (\phi \times r^2) - ((r-d) \times ((r^2) - (r-d)^2)^{1/2})$

Where:

- ϕ = angle (radians)
- r = radius (ft)
- d = depth of water in pipe



Output:

Field	1	2	3	4	5
SV (acre-ft)	0.0079	0.0118	0.0203	0.0287	0.0406
SV (gallons)	2584.2	3857.0	6609.1	9361.3	13218.3
SE (ft)	78.25	78.67	79.50	80.33	82.00

Hec-1 Analyses:

- 1.) *Cornell University 24-hour Precipitation Reference*
- 2.) *Existing Conditions Hec-1 Model*
- 3.) *Developed Conditions Hec-1 Model*

Extreme Precipitation Tables

Northeast Regional Climate Center

Data represents point estimates calculated from partial duration series. All precipitation amounts are displayed in inches.

Metadata for Point	
Smoothing	Yes
State	
Location	41.084 degrees North
Latitude	73.921 degrees West
Longitude	20 feet
Elevation	Wed Aug 07 2024 14:39:50 GMT-0400 (Eastern Daylight Time)
Date/Time	



Extreme Precipitation Estimates

	5min	10min	15min	30min	60min	120min	1hr	2hr	3hr	6hr	12hr	24hr	48hr	1day	2day
1yr	0.33	0.51	0.63	0.83	1.03	1.29	0.89	1.24	1.48	1.83	2.26	2.79	3.19	2.47	3.06
2yr	0.40	0.62	0.77	1.01	1.27	1.59	1.10	1.49	1.83	2.26	2.78	3.41	3.84	3.02	3.65
5yr	0.47	0.73	0.91	1.22	1.56	1.98	1.35	1.84	2.28	2.83	3.49	4.28	4.87	3.79	4.68
10yr	0.52	0.82	1.04	1.41	1.83	2.34	1.58	2.15	2.71	3.37	4.15	5.08	5.83	4.50	5.60
25yr	0.61	0.97	1.23	1.70	2.27	2.92	1.96	2.67	3.40	4.25	5.24	6.40	7.40	5.66	7.12
50yr	0.69	1.10	1.42	1.98	2.66	3.46	2.30	3.13	4.04	5.06	6.24	7.61	8.87	6.74	8.52
100yr	0.78	1.26	1.62	2.30	3.14	4.11	2.71	3.69	4.81	6.03	7.43	9.07	10.64	8.02	10.2
200yr	0.88	1.44	1.86	2.67	3.69	4.87	3.19	4.34	5.72	7.19	8.87	10.81	12.77	9.57	12.2
500yr	1.05	1.73	2.26	3.28	4.59	6.10	3.96	5.38	7.19	9.06	11.20	13.65	16.26	12.08	15.6

Lower Confidence Limits

	5min	10min	15min	30min	60min	120min	1hr	2hr	3hr	6hr	12hr	24hr	48hr	1day	2day
1yr	0.28	0.43	0.53	0.71	0.87	1.14	0.75	1.12	1.27	1.67	2.13	2.33	2.90	2.07	2.75

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
* MAY 1991 *
*
* VERSION 4.0.1U *
*
* Lahey F77L-EM/32 version 5.01 *
*
* Dodson & Associates, Inc. *
*
* RUN DATE 08/07/24 TIME 14:44:13 *
*
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 551-1748
*

```

92 CLINTON AVENUE #YB-2725: EXISTING CONDITIONS HEC-1 ANALYSIS

```

X X XXXXXXX XXXXX X
X X X X X XX
X X X X X X
XXXXXXX XXXX X XXXXX X
X X X X X X
X X X X X X
X X XXXXXXX XXXXX XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

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LINE ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1 ID -----input file:EX.ih1-----
2 ID
3 ID HYDROLOGY FOR: 92 CLINTON AVENUE YB-2725
4 ID TOWN OF RAMAPO, ROCKLAND COUNT
5 ID DATE: 8-7-24
6 ID
7 ID ANALYSIS PREPARED BY: SPARACO.& YOUNGBLOOD, PLLC
8 ID
9 ID ANALYSIS PARAMETERS:
10 ID EXISTING CONDITIONS RUN
11 ID STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
12 ID HYDROGRAPH METHOD: SCS
13 ID RAINFALL DISTRIBUTION: SCS TYPE III
14 ID
15 ID 24 HOUR RAINFALL DATA:
16 ID 1 YEAR: 2.79 INCHES
17 ID 2 YEAR: 3.41 INCHES
18 ID 5 YEAR: 4.28 INCHES
19 ID 10 YEAR: 5.08 INCHES
20 ID 25 YEAR: 6.40 INCHES
21 ID 100 YEAR: 9.07 INCHES
22 ID
23 ID
24 ID *DIAGRAM
24 IT 6 0 0 300
25 IO 3 0
26 JR PREC 2.79 3.41 4.28 5.08 6.4 9.07
27 KK SITE-1SITE RUNOFF TOWARD POINT#1
28 KM
29 KM *****
30 KM * DRAINAGE AREA = 0.44 AC = 0.0007 SQ. MI. CN=70 *
31 KM * TIME OF CONCENTRATION = 10.0 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.10 *
32 KM *****
33 KM
34 BA 0.0007
35 PB 1
36 IN 6
37 PC 0 0.001 0.002 0.003 0.004 0.005 0.006 0.007 0.008 0.009
38 PC 0.010 0.011 0.012 0.013 0.014 0.015 0.016 0.017 0.018 0.019
39 PC 0.020 0.021 0.022 0.023 0.024 0.026 0.027 0.028 0.029 0.030
40 PC 0.0305 0.031 0.032 0.034 0.035 0.036 0.037 0.038 0.040 0.041
41 PC 0.042 0.043 0.045 0.046 0.047 0.049 0.050 0.051 0.053 0.054
42 PC 0.055 0.057 0.058 0.060 0.061 0.063 0.064 0.066 0.067 0.069
43 PC 0.070 0.072 0.074 0.075 0.077 0.079 0.080 0.082 0.084 0.085
44 PC 0.087 0.089 0.091 0.093 0.095 0.097 0.100 0.103 0.106 0.109

```

45	PC	0.112	0.115	0.118	0.121	0.124	0.127	0.130	0.134	0.137	0.140
46	PC	0.144	0.148	0.151	0.155	0.159	0.163	0.167	0.171	0.176	0.180
47	PC	0.185	0.189	0.194	0.199	0.205	0.210	0.216	0.222	0.228	0.235
48	PC	0.242	0.250	0.258	0.266	0.276	0.287	0.298	0.312	0.328	0.363
49	PC	0.416	0.500	0.584	0.638	0.673	0.689	0.702	0.714	0.725	0.734
50	PC	0.743	0.751	0.758	0.766	0.772	0.779	0.785	0.790	0.796	0.801
51	PC	0.806	0.811	0.816	0.821	0.825	0.829	0.834	0.838	0.842	0.845
52	PC	0.849	0.853	0.857	0.860	0.864	0.867	0.870	0.874	0.877	0.880
53	PC	0.886	0.889	0.892	0.895	0.898	0.900	0.903	0.906	0.908	0.910

HEC-1 INPUT

PAGE 2

LINE	ID	1	2	3	4	5	6	7	8	9	10
54	PC	0.911	0.913	0.915	0.917	0.919	0.920	0.922	0.924	0.925	0.927
55	PC	0.929	0.930	0.932	0.933	0.935	0.936	0.938	0.939	0.941	0.942
56	PC	0.944	0.945	0.946	0.948	0.949	0.951	0.952	0.953	0.955	0.956
57	PC	0.957	0.958	0.960	0.961	0.962	0.963	0.965	0.966	0.967	0.968
58	PC	0.969	0.971	0.972	0.973	0.974	0.975	0.976	0.977	0.978	0.979
59	PC	0.981	0.982	0.983	0.984	0.985	0.986	0.987	0.988	0.989	0.990
60	PC	0.991	0.992	0.993	0.994	0.995	0.996	0.997	0.998	0.999	1.000
61	LS	1	70	0							
62	UD	0.1									
63	ZZ										

SCHEMATIC DIAGRAM OF STREAM NETWORK

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
 NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW
 27 SITE-1

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

 *
 * FLOOD HYDROGRAPH PACKAGE (HEC-1) *
 * MAY 1991 *
 * VERSION 4.0.1U *
 * Lahey F77L-EM/32 version 5.01 *
 * Dodson & Associates, Inc. *
 * RUN DATE 08/07/24 TIME 14:44:13 *

*
 * U.S. ARMY CORPS OF ENGINEERS *
 * HYDROLOGIC ENGINEERING CENTER *
 * 609 SECOND STREET *
 * DAVIS, CALIFORNIA 95616 *
 * (916) 551-1748 *

-----input file:EX.ih1-----

HYDROLOGY FOR: 92 CLINTON AVENUE YB-2725
 TOWN OF RAMAPO, ROCKLAND COUNT
 DATE: 8-7-24

ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC

ANALYSIS PARAMETERS:
 EXISTING CONDITIONS RUN
 STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
 HYDROGRAPH METHOD: SCS
 RAINFALL DISTRIBUTION: SCS TYPE III

24 HOUR RAINFALL DATA:
 1 YEAR: 2.79 INCHES
 2 YEAR: 3.41 INCHES
 5 YEAR: 4.28 INCHES
 10 YEAR: 5.08 INCHES
 25 YEAR: 6.40 INCHES
 100 YEAR: 9.07 INCHES

25 IO OUTPUT CONTROL VARIABLES
 IPRNT 3 PRINT CONTROL
 IPLOT 0 PLOT CONTROL
 QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
 NMIN 6 MINUTES IN COMPUTATION INTERVAL
 IDATE 1 0 STARTING DATE
 ITIME 0000 STARTING TIME
 NQ 300 NUMBER OF HYDROGRAPH ORDINATES
 NDDATE 2 0 ENDING DATE
 NDTIME 0554 ENDING TIME
 ICENT 19 CENTURY MARK

COMPUTATION INTERVAL 0.10 HOURS

TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS

DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-Feet
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
2.79 3.41 4.28 5.08 6.40 9.07

*** **

* *
27 KK * SITE-1 * SITE RUNOFF TOWARD POINT#1
* *

* DRAINAGE AREA = 0.44 AC = 0.0007 SQ. MI. CN=70 *
* TIME OF CONCENTRATION = 10.0 MIN = 0.167 HR x 0.6 (SCS LAG) = 0.10 *

36 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 6 TIME INTERVAL IN MINUTES
JXDATE 1 0 STARTING DATE
JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

34 BA SUBBASIN CHARACTERISTICS
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
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0.00 0.01 0.00 0.01 0.00 0.01 0.01 0.01 0.01 0.01
0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.01 0.02 0.03
0.08 0.08 0.05 0.03 0.02 0.01 0.01 0.01 0.01 0.01
0.01 0.01 0.01 0.01 0.01 0.01 0.00 0.01 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
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0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

61 LS SCS LOSS RATE
STRTL 1.00 INITIAL ABSTRACTION
CRVNBR 70.00 CURVE NUMBER
RTIMP 0.00 PERCENT IMPERVIOUS AREA

62 UD SCS DIMENSIONLESS UNITGRAPH
TLAG 0.10 LAG

UNIT HYDROGRAPH
7 END-OF-PERIOD ORDINATES
2. 2. 1. 0. 0. 0. 0.

TOTAL RAINFALL = 1.00, TOTAL LOSS = 1.00, TOTAL EXCESS = 0.00

PEAK FLOW TIME MAXIMUM AVERAGE FLOW
+ (CFS) (HR) 6-HR 24-HR 72-HR 29.90-HR

		(CFS)	0.	0.	0.	0.
+	0.	0.10	(INCHES) 0.000	0.000	0.000	0.000
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 2.79

TOTAL RAINFALL =		2.79,	TOTAL LOSS =	2.26,	TOTAL EXCESS =	0.53
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	0.	12.30	0.	0.	0.	0.
			(INCHES) 0.426	0.527	0.527	0.527
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 3.41

TOTAL RAINFALL =		3.41,	TOTAL LOSS =	2.54,	TOTAL EXCESS =	0.87
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	0.	12.30	0.	0.	0.	0.
			(INCHES) 0.716	0.867	0.867	0.867
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 4.28

TOTAL RAINFALL =		4.28,	TOTAL LOSS =	2.86,	TOTAL EXCESS =	1.42
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	1.	12.30	0.	0.	0.	0.
			(INCHES) 1.183	1.422	1.422	1.422
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 5.08

TOTAL RAINFALL =		5.08,	TOTAL LOSS =	3.09,	TOTAL EXCESS =	1.99
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	1.	12.30	0.	0.	0.	0.
			(INCHES) 1.657	1.990	1.990	1.990
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 6.40

TOTAL RAINFALL =		6.40,	TOTAL LOSS =	3.39,	TOTAL EXCESS =	3.01
PEAK FLOW	TIME			MAXIMUM AVERAGE FLOW		
			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)	(CFS)			
+	1.	12.30	0.	0.	0.	0.
			(INCHES) 2.499	3.011	3.011	3.011
			(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION SITE-1
FOR PLAN 1, RATIO = 9.07

TOTAL RAINFALL = 9.07, TOTAL LOSS = 3.80, TOTAL EXCESS = 5.27

PEAK FLOW (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
2.	12.20	0.	0.	0.	0.
		(INCHES) 4.331	5.271	5.271	5.271
		(AC-FT) 0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

1

PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
VOLUME IN ACRE-FEET, TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION					
				RATIO 1 2.79	RATIO 2 3.41	RATIO 3 4.28	RATIO 4 5.08	RATIO 5 6.40	RATIO 6 9.07
HYDROGRAPH AT +	SITE-1	0.001	1 FLOW	0.17	0.32	0.55	0.79	1.19	2.12
			TIME	12.30	12.30	12.30	12.30	12.30	12.20
			VOLUME	0.02	0.03	0.05	0.07	0.11	0.20

*** NORMAL END OF HEC-1 ***

```

1*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
*
*     MAY 1991 *
*
*     VERSION 4.0.1U *
*
*     Lahey F77L-EM/32 version 5.01 *
*
*     Dodson & Associates, Inc. *
*
* RUN DATE 08/07/24 TIME 15:11:34 *
*****
*****

```

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*
* U.S. ARMY CORPS OF ENGINEERS
*
* HYDROLOGIC ENGINEERING CENTER
*
* 609 SECOND STREET
*
* DAVIS, CALIFORNIA 95616
*
* (916) 551-1748
*

```

92 CLINTON AVENUE #YB-2725: DEVELOPED CONDITIONS HEC-1 ANALYSIS

```

X  X  XXXXXXX  XXXXX  X
X  X  X  X  X  XX
X  X  X  X  X  X
XXXXXXX  XXXX  X  XXXXX  X
X  X  X  X  X  X
X  X  X  X  X  X
X  X  XXXXXXX  XXXXX  -  XXX

```

THIS PROGRAM REPLACES ALL PREVIOUS VERSIONS OF HEC-1 KNOWN AS HEC1 (JAN 73), HEC1GS, HEC1DB, AND HEC1KW.

THE DEFINITIONS OF VARIABLES -RTIMP- AND -RTIOR- HAVE CHANGED FROM THOSE USED WITH THE 1973-STYLE INPUT STRUCTURE. THE DEFINITION OF -AMSKK- ON RM-CARD WAS CHANGED WITH REVISIONS DATED 28 SEP 81. THIS IS THE FORTRAN77 VERSION NEW OPTIONS: DAMBREAK OUTFLOW SUBMERGENCE , SINGLE EVENT DAMAGE CALCULATION, DSS:WRITE STAGE FREQUENCY, DSS:READ TIME SERIES AT DESIRED CALCULATION INTERVAL LOSS RATE:GREEN AND AMPT INFILTRATION KINEMATIC WAVE: NEW FINITE DIFFERENCE ALGORITHM

1

HEC-1 INPUT

PAGE 1

```

LINE      ID.....1.....2.....3.....4.....5.....6.....7.....8.....9.....10
1          ID          ~~~~~input file:DEV.ih1~~~~~
2          ID
3          ID          HYDROLOGY FOR: 92 CLINTON AVENUE YB-2725
4          ID          TOWN OF RAMAPO, ROCKLAND COUNT
5          ID          DATE: 8-7-24
6          ID
7          ID          ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC
8          ID
9          ID          ANALYSIS PARAMETERS:
10         ID          DEVELOPED CONDITIONS RUN
11         ID          STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
12         ID          HYDROGRAPH METHOD:          SCS
13         ID          RAINFALL DISTRIBUTION:      SCS TYPE III
14         ID
15         ID          24 HOUR RAINFALL DATA:
16         ID          1 YEAR: 2.79 INCHES
17         ID          2 YEAR: 3.41 INCHES
18         ID          5 YEAR: 4.28 INCHES
19         ID          10 YEAR: 5.08 INCHES
20         ID          25 YEAR: 6.40 INCHES
21         ID          100 YEAR: 9.07 INCHES
22         ID
23         ID
24         ID          *DIAGRAM
25         ID          IT          6          0          0          300
26         ID          IO          3          0
27         ID          JR          PREC          2.79          3.41          4.28          5.08          6.4          9.07
28         ID
29         ID          KK          SITE-1SITE RUNOFF TOWARD POINT#1
30         ID          KM
31         ID          KM          *****
32         ID          KM          * DRAINAGE AREA = 0.16 AC = 0.0003 SQ. MI.          CN=74          *
33         ID          KM          * TIME OF CONCENTRATION = 5.0 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.05          *
34         ID          KM          *****
35         ID          BA          0.0003
36         ID          PB          1
37         ID          IN          6
38         ID          PC          0          0.001          0.002          0.003          0.004          0.005          0.006          0.007          0.008          0.009
39         ID          PC          0.010          0.011          0.012          0.013          0.014          0.015          0.016          0.017          0.018          0.019
40         ID          PC          0.020          0.021          0.022          0.023          0.024          0.026          0.027          0.028          0.029          0.030
41         ID          PC          0.0305          0.031          0.032          0.034          0.035          0.036          0.037          0.038          0.040          0.041
42         ID          PC          0.042          0.043          0.045          0.046          0.047          0.049          0.050          0.051          0.053          0.054
43         ID          PC          0.055          0.057          0.058          0.060          0.061          0.063          0.064          0.066          0.067          0.069
44         ID          PC          0.070          0.072          0.074          0.075          0.077          0.079          0.080          0.082          0.084          0.085
45         ID          PC          0.087          0.089          0.091          0.093          0.095          0.097          0.100          0.103          0.106          0.109

```

45	PC	0.112	0.115	0.118	0.121	0.124	0.127	0.130	0.134	0.137	0.140
46	PC	0.144	0.148	0.151	0.155	0.159	0.163	0.167	0.171	0.176	0.180
47	PC	0.185	0.189	0.194	0.199	0.205	0.210	0.216	0.222	0.228	0.235
48	PC	0.242	0.250	0.258	0.266	0.276	0.287	0.298	0.312	0.328	0.363
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50	PC	0.743	0.751	0.758	0.766	0.772	0.779	0.785	0.790	0.796	0.801
51	PC	0.806	0.811	0.816	0.821	0.825	0.829	0.834	0.838	0.842	0.845
52	PC	0.849	0.853	0.857	0.860	0.864	0.867	0.870	0.874	0.877	0.880
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HEC-1 INPUT

PAGE 2

1

LINE	ID	1	2	3	4	5	6	7	8	9	10
54	PC	0.911	0.913	0.915	0.917	0.919	0.920	0.922	0.924	0.925	0.927
55	PC	0.929	0.930	0.932	0.933	0.935	0.936	0.938	0.939	0.941	0.942
56	PC	0.944	0.945	0.946	0.948	0.949	0.951	0.952	0.953	0.955	0.956
57	PC	0.957	0.958	0.960	0.961	0.962	0.963	0.965	0.966	0.967	0.968
58	PC	0.969	0.971	0.972	0.973	0.974	0.975	0.976	0.977	0.978	0.979
59	PC	0.981	0.982	0.983	0.984	0.985	0.986	0.987	0.988	0.989	0.990
60	PC	0.991	0.992	0.993	0.994	0.995	0.996	0.997	0.998	0.999	1.000
61	LS	1	74	0							
62	UD	0.05									
63	KK	SITE2DEV. SITE-2 TO UNDERGROUND STORAGE									
64	KM	*****									
65	KM	*****									
66	KM	* DRAINAGE AREA = 0.28 AC = 0.0004 SQ. MI. CN=83 *									
67	KM	* TIME OF CONCENTRATION = 5.0 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *									
68	KM	*****									
69	KM	*****									
70	BA	0.0004									
71	LS	1	83								
72	UD	0.05									
73	KK	ROUTEROUTING IN UNDERGROUND STORAGE SYSTEM									
74	KM	*****									
75	KM	OUTLET STRUCTURE DATA: 90 LF OF 60" DIA. PIPE									
76	KM	*****									
77	KM	* WEIR LENGTH = 3.14' (12" RISER) WEIR OVERFLOW AT EL.: 81.0 *									
78	KM	* 2.25-INCH DIAMETER ORIFICE AT EL. 77.0 *									
79	KM	*****									
80	KM	*****									
81	RS	1	ELEV	77							
82	SV	0	0.0079	0.0118	0.0203	0.0287	0.0406	0.0406			
83	SE	77	78.25	78.67	79.5	80.33	82	84			
84	SL	77.09	0.0276	0.6	0.5						
85	SS	81.5	3.14	3.0	1.5						
86	ST	83.2	10	3.0	1.5						
87	KK	PT.1COMBINE SITE-1 AND ROUTE HYDROGRAPHS									
88	HC	2									
89	ZZ										

1

SCHEMATIC DIAGRAM OF STREAM NETWORK

```

INPUT LINE (V) ROUTING (--->) DIVERSION OR PUMP FLOW
NO. (.) CONNECTOR (<---) RETURN OF DIVERTED OR PUMPED FLOW

27 SITE-1
.
.
63 . SITE2
. V
. V
73 . ROUTE
.
.
87 PT.1.....

```

(***) RUNOFF ALSO COMPUTED AT THIS LOCATION

```

*****
*****
*
* FLOOD HYDROGRAPH PACKAGE (HEC-1) *
* MAY 1991 *
* VERSION 4.0.1U *
* Lahey F77L-EM/32 version 5.01 *
* Dodson & Associates, Inc. *
* RUN DATE 08/07/24 TIME 15:11:34 *
*****
*****

```

```

*
* U.S. ARMY CORPS OF ENGINEERS
* HYDROLOGIC ENGINEERING CENTER
* 609 SECOND STREET
* DAVIS, CALIFORNIA 95616
* (916) 551-1748
*

```

-----input file:DEV.ih1-----

HYDROLOGY FOR: 92 CLINTON AVENUE YB-2725
TOWN OF RAMAPO, ROCKLAND COUNT
DATE: 8-7-24

ANALYSIS PREPARED BY: SPARACO & YOUNGBLOOD, PLLC

ANALYSIS PARAMETERS:
DEVELOPED CONDITIONS RUN
STORM RECURRENCE INTERVALS = 1, 2, 5, 10, 25 & 100 YEAR
HYDROGRAPH METHOD: SCS
RAINFALL DISTRIBUTION: SCS TYPE III

24 HOUR RAINFALL DATA:
1 YEAR: 2.79 INCHES
2 YEAR: 3.41 INCHES
5 YEAR: 4.28 INCHES
10 YEAR: 5.08 INCHES
25 YEAR: 6.40 INCHES
100 YEAR: 9.07 INCHES

25 IO OUTPUT CONTROL VARIABLES
IPRNT 3 PRINT CONTROL
IPLOT 0 PLOT CONTROL
QSCAL 0. HYDROGRAPH PLOT SCALE

IT HYDROGRAPH TIME DATA
NMIN 6 MINUTES IN COMPUTATION INTERVAL
IDATE 1 0 STARTING DATE
ITIME 0000 STARTING TIME
NQ 300 NUMBER OF HYDROGRAPH ORDINATES
NDDATE 2 0 ENDING DATE
NDTIME 0554 ENDING TIME
ICENT 19 CENTURY MARK
COMPUTATION INTERVAL 0.10 HOURS
TOTAL TIME BASE 29.90 HOURS

ENGLISH UNITS
DRAINAGE AREA SQUARE MILES
PRECIPITATION DEPTH INCHES
LENGTH, ELEVATION FEET
FLOW CUBIC FEET PER SECOND
STORAGE VOLUME ACRE-FEET
SURFACE AREA ACRES
TEMPERATURE DEGREES FAHRENHEIT

JP MULTI-PLAN OPTION
NPLAN 1 NUMBER OF PLANS

JR MULTI-RATIO OPTION
RATIOS OF PRECIPITATION
2.79 3.41 4.28 5.08 6.40 9.07

*** **

27 KK *****
* SITE-1 * SITE RUNOFF TOWARD POINT#1

* DRAINAGE AREA = 0.16 AC = 0.0003 SQ. MI. CN=74 *
* TIME OF CONCENTRATION = 5.0 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.05 *

36 IN TIME DATA FOR INPUT TIME SERIES
JXMIN 6 TIME INTERVAL IN MINUTES
JXDATE 1 0 STARTING DATE
JXTIME 0 STARTING TIME

SUBBASIN RUNOFF DATA

34 BA SUBBASIN CHARACTERISTICS
TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

(AC-FT) 0. 0. 0. 0.
 CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION SITE-1
 FOR PLAN 1, RATIO = 5.08

TOTAL RAINFALL = 5.08, TOTAL LOSS = 2.89, TOTAL EXCESS = 2.19

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
0.	12.20	0.	0.	0.	0.
		(INCHES) 1.833	2.192	2.192	2.192
		(AC-FT) 0.	0.	0.	0.
		CUMULATIVE AREA = 0.00 SQ MI			

*** **

HYDROGRAPH AT STATION SITE-1
 FOR PLAN 1, RATIO = 6.40

TOTAL RAINFALL = 6.40, TOTAL LOSS = 3.13, TOTAL EXCESS = 3.27

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	12.20	0.	0.	0.	0.
		(INCHES) 2.727	3.271	3.271	3.271
		(AC-FT) 0.	0.	0.	0.
		CUMULATIVE AREA = 0.00 SQ MI			

*** **

HYDROGRAPH AT STATION SITE-1
 FOR PLAN 1, RATIO = 9.07

TOTAL RAINFALL = 9.07, TOTAL LOSS = 3.45, TOTAL EXCESS = 5.62

PEAK FLOW + (CFS)	TIME (HR)	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
1.	12.20	0.	0.	0.	0.
		(INCHES) 4.625	5.622	5.622	5.622
		(AC-FT) 0.	0.	0.	0.
		CUMULATIVE AREA = 0.00 SQ MI			

*** **

63 KK SITE2 DEV. SITE-2 TO UNDERGROUND STORAGE

 * DRAINAGE AREA = 0.28 AC = 0.0004 SQ. MI. CN=83 *
 * TIME OF CONCENTRATION = 5.0 MIN = 0.083 HR x 0.6 (SCS LAG) = 0.050 *

SUBBASIN RUNOFF DATA

70 BA SUBBASIN CHARACTERISTICS
 TAREA 0.00 SUBBASIN AREA

PRECIPITATION DATA

35 PB STORM 1.00 BASIN TOTAL PRECIPITATION

37 PI INCREMENTAL PRECIPITATION PATTERN

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.01	0.00	0.01	0.00	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.02	0.03	0.05
0.08	0.08	0.05	0.03	0.02	0.01	0.01	0.01	0.01	0.01	0.01
0.01	0.01	0.01	0.01	0.01	0.01	0.01	0.00	0.01	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00
0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00

71 LS SCS LOSS RATE
 STRTL 1.00 INITIAL ABSTRACTION
 CRVNBR 83.00 CURVE NUMBER
 RTIMP 0.00 PERCENT IMPERVIOUS AREA

72 UD SCS DIMENSIONLESS UNITGRAPH
 TLAG 0.05 LAG

UNIT HYDROGRAPH
 5 END-OF-PERIOD ORDINATES

2.	1.	0.	0.	0.	
TOTAL RAINFALL =	1.00,	TOTAL LOSS =	1.00,	TOTAL EXCESS =	0.00
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)		6-HR	24-HR	72-HR
+ 0.	0.10	(CFS)	0.	0.	0.
		(INCHES)	0.000	0.000	0.000
		(AC-FT)	0.	0.	0.
		CUMULATIVE AREA =	0.00	SQ MI	

HYDROGRAPH AT STATION SITE2
 FOR PLAN 1, RATIO = 2.79

TOTAL RAINFALL =	2.79,	TOTAL LOSS =	1.96,	TOTAL EXCESS =	0.83
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)		6-HR	24-HR	72-HR
+ 0.	12.20	(CFS)	0.	0.	0.
		(INCHES)	0.690	0.835	0.835
		(AC-FT)	0.	0.	0.
		CUMULATIVE AREA =	0.00	SQ MI	

HYDROGRAPH AT STATION SITE2
 FOR PLAN 1, RATIO = 3.41

TOTAL RAINFALL =	3.41,	TOTAL LOSS =	2.11,	TOTAL EXCESS =	1.30
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)		6-HR	24-HR	72-HR
+ 0.	12.20	(CFS)	0.	0.	0.
		(INCHES)	1.098	1.303	1.303
		(AC-FT)	0.	0.	0.
		CUMULATIVE AREA =	0.00	SQ MI	

HYDROGRAPH AT STATION SITE2
 FOR PLAN 1, RATIO = 4.28

TOTAL RAINFALL =	4.28,	TOTAL LOSS =	2.26,	TOTAL EXCESS =	2.02
PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW		
+ (CFS)	(HR)		6-HR	24-HR	72-HR
+ 1.	12.20	(CFS)	0.	0.	0.
		(INCHES)	1.711	2.019	2.019
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION SITE2
FOR PLAN 1, RATIO = 5.08

TOTAL RAINFALL = 5.08, TOTAL LOSS = 2.36, TOTAL EXCESS = 2.72

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	2.296	2.716	2.716	2.716
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION SITE2
FOR PLAN 1, RATIO = 6.40

TOTAL RAINFALL = 6.40, TOTAL LOSS = 2.48, TOTAL EXCESS = 3.92

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
1.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	3.290	3.915	3.915	3.915
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION SITE2
FOR PLAN 1, RATIO = 9.07

TOTAL RAINFALL = 9.07, TOTAL LOSS = 2.63, TOTAL EXCESS = 6.44

PEAK FLOW (CFS)	TIME (HR)		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
2.	12.20	(CFS)	0.	0.	0.	0.
		(INCHES)	5.299	6.436	6.436	6.436
		(AC-FT)	0.	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

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*
* 73 KK ROUTE * ROUTING IN UNDERGROUND STORAGE SYSTEM
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OUTLET STRUCTURE DATA: 90 LF OF 60" DIA. PIPE
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* WEIR LENGTH = 3.14' (12" RISER) WEIR OVERFLOW AT EL.: 81.0 *
* 2.25-INCH DIAMETER ORIFICE AT EL. 77.0 *
*****

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HYDROGRAPH ROUTING DATA

81 RS	STORAGE ROUTING							
	NSTPS	1	NUMBER OF SUBREACHES					
	ITYP	ELEV	TYPE OF INITIAL CONDITION					
	RSVRIC	77.00	INITIAL CONDITION					
	X	0.00	WORKING R AND D COEFFICIENT					
82 SV	STORAGE	0.0	0.0	0.0	0.0	0.0	0.0	0.0
83 SE	ELEVATION	77.00	78.25	78.67	79.50	80.33	82.00	84.00
84 SL	LOW-LEVEL OUTLET							
	ELEVL	77.09'	ELEVATION AT CENTER OF OUTLET					
	CAREA	0.03	CROSS-SECTIONAL AREA					
	COQL	0.60	COEFFICIENT					
	EXPL	0.50	EXPONENT OF HEAD					
85 SS	SPILLWAY							

CREL 81.50 SPILLWAY CREST ELEVATION
 SPWID 3.14 SPILLWAY WIDTH
 COQW 3.00 WEIR COEFFICIENT
 EXPW 1.50 EXPONENT OF HEAD

86 ST TOP OF DAM
 TOPEL 83.20 ELEVATION AT TOP OF DAM
 DAMWID 10.00 DAM WIDTH
 COQD 3.00 WEIR COEFFICIENT
 EXPD 1.50 EXPONENT OF HEAD

COMPUTED OUTFLOW-ELEVATION DATA

(EXCLUDING FLOW OVER DAM)

OUTFLOW	0.00	0.00	0.04	0.05	0.06	0.07	0.08	0.11	0.15	0.28
ELEVATION	77.00	77.09	77.19	77.22	77.26	77.34	77.47	77.73	78.44	81.50
OUTFLOW	0.32	0.59	1.30	2.69	4.97	8.37	13.11	19.41	27.49	37.58
ELEVATION	81.53	81.60	81.73	81.90	82.13	82.40	82.73	83.10	83.53	84.00

COMPUTED STORAGE-OUTFLOW-ELEVATION DATA

(INCLUDING FLOW OVER DAM)

STORAGE	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.00	0.01	0.01
OUTFLOW	0.00	0.00	0.04	0.05	0.06	0.07	0.08	0.11	0.14	0.15
ELEVATION	77.00	77.09	77.19	77.22	77.26	77.34	77.47	77.73	78.25	78.44
STORAGE	0.01	0.02	0.03	0.04	0.04	0.04	0.04	0.04	0.04	0.04
OUTFLOW	0.17	0.21	0.24	0.28	0.32	0.59	1.30	2.69	3.62	4.97
ELEVATION	78.67	79.50	80.33	81.50	81.53	81.60	81.73	81.90	82.00	82.13
STORAGE	0.04	0.04	0.04	0.04	0.04					
OUTFLOW	8.37	13.11	19.41	33.07	59.05					
ELEVATION	82.40	82.73	83.10	83.53	84.00					

*** **

HYDROGRAPH AT STATION ROUTE
 FOR PLAN 1, RATIO = 2.79

PEAK OUTFLOW IS 0. AT TIME 12.50 HOURS

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR
+	0.	0.	0.	0.	0.	0.
	12.50	(INCHES)	0.663	0.803	0.803	0.803
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	0.		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	77.54		77.17	77.09	77.07	77.07

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION ROUTE
 FOR PLAN 1, RATIO = 3.41

PEAK OUTFLOW IS 0. AT TIME 12.50 HOURS

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
(CFS)	(HR)	(CFS)	6-HR	24-HR	72-HR	29.90-HR
+	0.	0.	0.	0.	0.	0.
	12.50	(INCHES)	1.072	1.270	1.270	1.270
		(AC-FT)	0.	0.	0.	0.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
(AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	0.		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
(FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+	78.06		77.29	77.12	77.09	77.09

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION ROUTE
FOR PLAN 1, RATIO = 4.28

PEAK OUTFLOW IS 0. AT TIME 12.50 HOURS

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 0.	12.50	(INCHES)	0.	0.	0.	0.
		(AC-FT)	1.709	1.994	1.994	1.994
			0.	0.	0.	0.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 0.	12.40		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 78.75	12.50		77.55	77.19	77.15	77.15

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION ROUTE
FOR PLAN 1, RATIO = 5.08

PEAK OUTFLOW IS 0. AT TIME 12.50 HOURS

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 0.	12.50	(INCHES)	0.	0.	0.	0.
		(AC-FT)	2.296	2.690	2.690	2.690
			0.	0.	0.	0.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 0.	12.50		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 79.33	12.50		77.85	77.27	77.21	77.21

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION ROUTE
FOR PLAN 1, RATIO = 6.40

PEAK OUTFLOW IS 0. AT TIME 12.60 HOURS

PEAK FLOW	TIME		MAXIMUM AVERAGE FLOW			
			6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)	(CFS)				
+ 0.	12.50	(INCHES)	0.	0.	0.	0.
		(AC-FT)	3.275	3.887	3.887	3.887
			0.	0.	0.	0.
PEAK STORAGE	TIME		MAXIMUM AVERAGE STORAGE			
+ (AC-FT)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 0.	12.50		0.	0.	0.	0.
PEAK STAGE	TIME		MAXIMUM AVERAGE STAGE			
+ (FEET)	(HR)		6-HR	24-HR	72-HR	29.90-HR
+ 80.41	12.60		78.47	77.43	77.34	77.34

CUMULATIVE AREA = 0.00 SQ MI

*** *** *** *** ***

HYDROGRAPH AT STATION ROUTE
FOR PLAN 1, RATIO = 9.07

PEAK OUTFLOW IS 1. AT TIME 12.30 HOURS

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 1.	12.30	0.	0.	0.	0.
		(INCHES)	5.181	6.412	6.412
		(AC-FT)	0.	0.	0.

PEAK STORAGE	TIME	MAXIMUM AVERAGE STORAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (AC-FT)	(HR)				
+ 0.	12.30	0.	0.	0.	0.

PEAK STAGE	TIME	MAXIMUM AVERAGE STAGE			
		6-HR	24-HR	72-HR	29.90-HR
+ (FEET)	(HR)				
+ 81.71	12.30	79.37	77.68	77.55	77.55

CUMULATIVE AREA = 0.00 SQ MI

*** **

 * *
 87 KK * PT.1 * COMBINE SITE-1 AND ROUTE HYDROGRAPHS
 * *

88 HC HYDROGRAPH COMBINATION
 ICOMP 2 NUMBER OF HYDROGRAPHS TO COMBINE

*** **

HYDROGRAPH AT STATION PT.1
 FOR PLAN 1, RATIO = 2.79

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 0.	12.30	0.	0.	0.	0.
		(INCHES)	0.588	0.718	0.718
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION PT.1
 FOR PLAN 1, RATIO = 3.41

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 0.	12.30	0.	0.	0.	0.
		(INCHES)	0.961	1.146	1.146
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION PT.1
 FOR PLAN 1, RATIO = 4.28

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
		6-HR	24-HR	72-HR	29.90-HR
+ (CFS)	(HR)				
+ 0.	12.20	0.	0.	0.	0.
		(INCHES)	1.544	1.818	1.818
		(AC-FT)	0.	0.	0.

CUMULATIVE AREA = 0.00 SQ MI

*** **

HYDROGRAPH AT STATION PT.1
 FOR PLAN 1, RATIO = 5.08

PEAK FLOW	TIME	MAXIMUM AVERAGE FLOW			
-----------	------	----------------------	--	--	--

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	1.	12.20	0.	0.	0.	0.
		(CFS)				
		(INCHES)	2.098	2.476	2.476	2.476
		(AC-FT)	0.	0.	0.	0.
		CUMULATIVE AREA =	0.00 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION PT.1
FOR PLAN 1, RATIO = 6.40

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	1.	12.20	0.	0.	0.	0.
		(CFS)				
		(INCHES)	3.038	3.623	3.623	3.623
		(AC-FT)	0.	0.	0.	0.
		CUMULATIVE AREA =	0.00 SQ MI			

*** *** *** *** ***

HYDROGRAPH AT STATION PT.1
FOR PLAN 1, RATIO = 9.07

			6-HR	24-HR	72-HR	29.90-HR
+	(CFS)	(HR)				
+	2.	12.30	0.	0.	0.	0.
		(CFS)				
		(INCHES)	4.927	6.074	6.074	6.074
		(AC-FT)	0.	0.	0.	0.
		CUMULATIVE AREA =	0.00 SQ MI			

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PEAK FLOW AND STAGE (END-OF-PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND, AREA IN SQUARE MILES
VOLUME IN ACRE-FEET, TIME TO PEAK IN HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO PRECIPITATION						
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	
				2.79	3.41	4.28	5.08	6.40	9.07	
HYDROGRAPH AT	SITE-1	0.000	1	FLOW	0.09	0.18	0.30	0.43	0.65	1.10
+				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.01	0.02	0.03	0.04	0.05	0.09
HYDROGRAPH AT	SITE2	0.000	1	FLOW	0.19	0.34	0.55	0.74	1.06	1.68
+				TIME	12.20	12.20	12.20	12.20	12.20	12.20
				VOLUME	0.02	0.03	0.04	0.06	0.08	0.14
ROUTED TO	ROUTE	0.000	1	FLOW	0.09	0.13	0.17	0.20	0.24	1.16
+				TIME	12.50	12.50	12.50	12.50	12.50	12.30
				VOLUME	0.02	0.03	0.04	0.06	0.08	0.14
				** PEAK STAGES IN FEET **						
			1	STAGE	77.54	78.06	78.75	79.33	80.41	81.71
				TIME	12.50	12.50	12.50	12.50	12.60	12.30
2 COMBINED AT	PT.1	0.001	1	FLOW	0.17	0.27	0.44	0.59	0.84	2.02
+				TIME	12.30	12.30	12.20	12.20	12.20	12.30
				VOLUME	0.03	0.04	0.07	0.09	0.14	0.23

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SUMMARY OF DAM OVERTOPPING/BREACH ANALYSIS FOR STATION ROUTE
(PEAKS SHOWN ARE FOR INTERNAL TIME STEP USED DURING BREACH FORMATION)

PLAN 1		INITIAL VALUE	SPILLWAY CREST	TOP OF DAM				
	ELEVATION	77.00	81.50	83.20				
	STORAGE	0.	0.	0.				
	OUTFLOW	0.	0.	21.				
	RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF MAX OUTFLOW HOURS	TIME OF FAILURE HOURS
	2.79	77.54	0.00	0.	0.	0.00	12.50	0.00
	3.41	78.06	0.00	0.	0.	0.00	12.50	0.00
	4.28	78.75	0.00	0.	0.	0.00	12.50	0.00
	5.08	79.33	0.00	0.	0.	0.00	12.50	0.00
	6.40	80.41	0.00	0.	0.	0.00	12.60	0.00
	9.07	81.71	0.00	0.	1.	0.00	12.30	0.00